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## Active Control of Separation on a Wing with Oscillating Camber

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### Nomenclature

$c$	= chord length, 20.3 cm
$f$	= actuation frequency, Hz
$f^+$	= reduced frequency, $f \cdot c/U$
$Re$	= Reynolds number based on $c$
$U$	= freestream velocity
$\alpha$	= angle of attack, deg

### Introduction

**L**OW-REYNOLDS-NUMBER effects are significant in the aerodynamics of low-speed airfoils, aircraft intended to operate in low-density environments, and small-scale lifting surfaces such as insect and bird wings. Current aerodynamic applications include micro-aerial vehicles and unmanned aerial vehicles, as well as aircraft operating at high altitudes or low-density atmospheres other than Earth's.

The primary difficulty with the operation of a wing at low Reynolds number is that the flow over the suction surface encounters an adverse pressure gradient at a point at which the boundary layer is quite likely to still be laminar. Because a laminar boundary layer is incapable of negotiating any but the slightest adverse pressure gradient, the flow will inevitably separate. The separated flow then transitions to turbulence, entrains fluid, and reattaches to form a turbulent boundary layer. The resulting structure is the laminar separation bubble, which has been described by Lissaman.<sup>1</sup>

A number of different flow-control approaches have been investigated to reduce separation and improve efficiency at low Reynolds numbers.<sup>2</sup> Continuous blowing and sucking have long been shown to have pronounced effects. More recently, intermittent blowing and sucking in the form of synthetic jets have shown their effectiveness and suggest the presence of optimum values in the range of frequency inputs, which can translate to other oscillatory inputs.<sup>3–5</sup> Mechanical momentum transfer and acoustic excitation have also been explored.

The approach presented herein employs an adaptive wing.<sup>6</sup> Naturally, all practical wings are adaptive in the sense that they use actuators to alter lift coefficient by changing effective profile with a subsequent loss in efficiency. A truly adaptive wing, however, refers to an airfoil, which can change its profile to adapt optimally to flow conditions. Similar concepts have been explored in the past, such as the snap-through airfoil, which changes local airfoil camber by moving a flexible portion of the pressure surface<sup>7</sup> or the Defense Advanced Research Projects Agency "smart wing," which uses torsional elements to twist the wing.<sup>8</sup> Modern smart materials such as piezoelectric actuators offer great promise in the area of future stall

control applications,<sup>9</sup> although simple mechanisms such as buzzing bars have also been shown to be adequate stall control devices.<sup>10</sup> The kind of adaptation, which is of interest here, is one in which the rate of actuation is rapid and might be able to respond quickly enough to arrest or limit the formation of laminar separation bubbles. At high Reynolds numbers the unsteady theory of Theodorsen<sup>11</sup> can be used to solve such problems (for an example, see Duffy et al.<sup>12</sup>), but at low Reynolds numbers where viscous forces are predominate there is no rigorous method to predict the unsteady effects of such rapid actuation and how it will alter separation.

### Experiment

The adaptive wing design is based upon a static prototype design constructed by Pinkerton and Moses as a feasibility test for drag reduction.<sup>13</sup> A modular wing was constructed with a base profile of a NACA 4415. Each module has a recess cut in the upper surface into which a piezoelectric actuator is placed. The actuators are mounted at such an angle that they are even with the unrecessed airfoil section when at their smallest effective radius (when most curved). A thin plastic sheet is then placed over the actuator to smooth the profile, and then the entire assembly is wrapped in a latex membrane to hold it together and provide a seamless outer surface. When the actuator is displaced to its greatest effective radius (closest to being flat), it protrudes through the upper cross section. The plastic sheet and latex membrane smooth the upper surface, increasing the effective camber and moving the point of maximum thickness aft. The device has been more fully described elsewhere.<sup>14</sup>

Experiments with a circular-arc airfoil at low Reynolds number suggest that an airfoil with oscillating camber will produce a higher lift coefficient than the same airfoil at any fixed camber setting through separation control.<sup>15</sup> The present experiment attempts to extend this finding to airfoils of more ordinary and more efficient cross section. The current experiments were conducted with four wing modules, assembled to form a wing with a chord of 8 in. (203 mm) and a span of 13 in. (330 mm), giving an aspect ratio of 1.6. This wing was mounted in an 8 × 16-in. (203 × 406 mm) test section in a low-speed low-turbulence wind tunnel. Smoke-wire flow visualization as described in Batill and Mueller is used to mark the outer boundary of separated flow.<sup>16</sup> Displacement of the actuators was measured in situ with a Keyence LK-501 laser displacement sensor. These measurements are accurate to within ±5% at all frequencies across the range of interest.

### Results

Flow visualization at  $Re = 2.5 \times 10^4$  and  $5.0 \times 10^4$  clearly shows large separated flow over the wing with the actuator static ( $f^+ = 0$ ). This is expected at low speeds with a NACA 4415 profile, which is not designed for low-Reynolds-number flight. When the actuator is oscillating, the size of the separated flow is greatly reduced. Figure 1 shows images of the flow visualization for  $Re = 2.5 \times 10^4$  at two different angles of attack for both uncontrolled and controlled runs where  $f^+ = 0$  and  $f^+ > 0$ , respectively. From the recorded images the size of the separated region at 70% of chord was measured normal to the surface of the foil by determining the distance from the airfoil surface to the mean location of the first smoke streakline. These measurements are presented in Figs. 2 and 3. The instrumental error in these measurements amounts to ±0.2 mm or far less than 1% of chord. This is dwarfed by the statistical error, which can best be inferred from examining the scatter in the dynamic data (variation in streakline location). The overall error, then, is within ±1% of chord.

The static measurements refer to those where the actuator was kept in a stationary state at a number of predetermined positions. For these an increase in separation as angle of attack increases is seen, which is what would be expected. An increase in separation as Reynolds number decreases is also seen. This is also as one would expect. The main purpose of the static measurements was to provide a direct comparison to the dynamic measurements. To that end the minimum size observed is the value used in Fig. 4, which represents a best-case scenario for separated flow over an unactuated airfoil.

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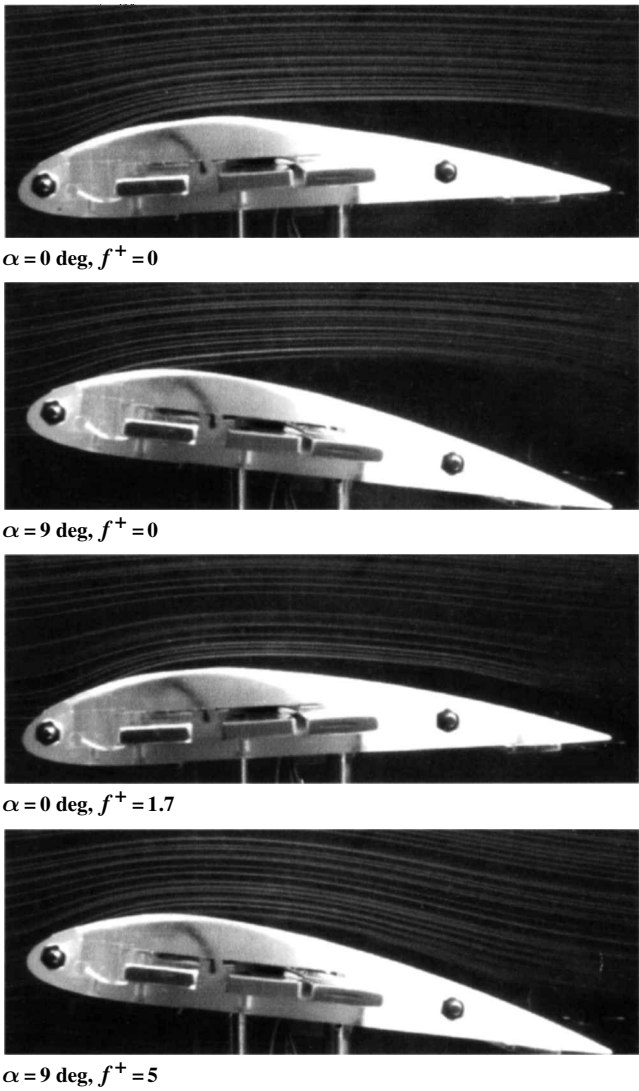


Fig. 1 Smoke-wire flow visualization at  $Re = 2.5 \times 10^4$  for static and actuated cases.

Force and particle image velocimetry (PIV) measurements of the airfoil with static shape changes were studied at a preliminary stage using solid models over a range of overlapping Reynolds number corresponding to the flow-visualization observations shown in Fig. 2 (Ref. 17). Force measurements showed that both coefficients of lift and drag showed a slight increase at intermediate settings of the actuator, with an overall decrease in the lift-to-drag ratio (L/D) of 6%. Maximum actuator displacement also increased both lift and drag but with an overall increase in L/D of 2%. This was confirmed in the PIV measurements, where it was revealed that the size of the separation region increased and then decreased with increasing static actuator position. The modest improvement in efficiency did not warrant further investigation of static actuator effects, however. Moment coefficients were not measured.

The dynamic measurements refer to those in which the actuator was oscillated at a given frequency. The amplitude of oscillation was normalized to  $\pm 0.2$  mm measured at  $0.3c$ . This represents a peak-to-peak displacement of  $0.002c$ . For frequencies above 70 Hz, this normalization could not be maintained without producing destructive sparks along the edges of the actuator or at the attachment points of the electrical leads. Measurements above this frequency were taken with reduced maximum displacement. The regions of normalized displacement and non-normalized displacement are noted on Fig. 3. The data are plotted in terms of reduced frequency  $f^+$ , where frequency is normalized by chord length and freestream velocity,  $f^+ = f \cdot c / U$ .

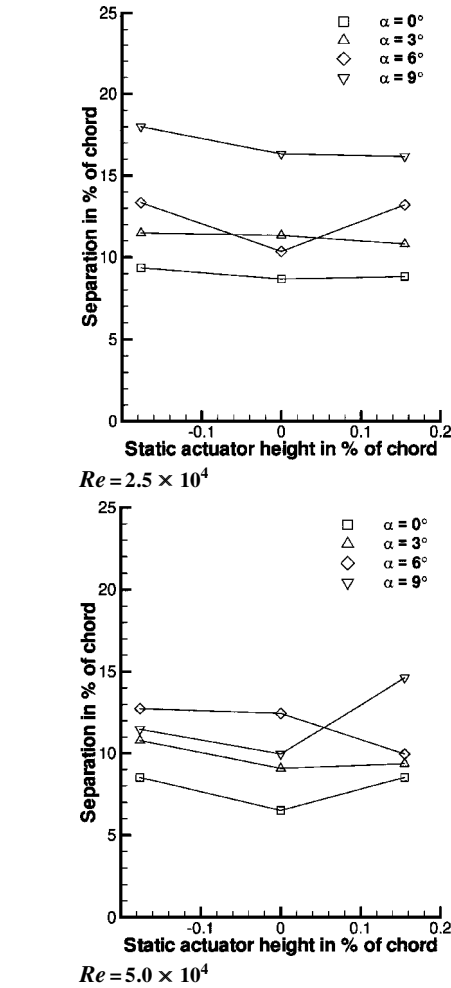


Fig. 2 Separated flow thickness measured normal to the suction surface at 70% of chord for the static case.

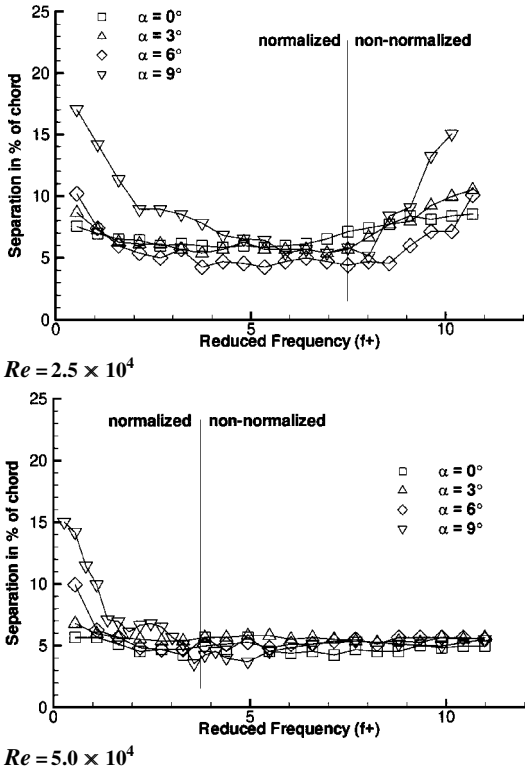


Fig. 3 Separated flow thickness measured normal to the suction surface at 70% of chord for the dynamic case.

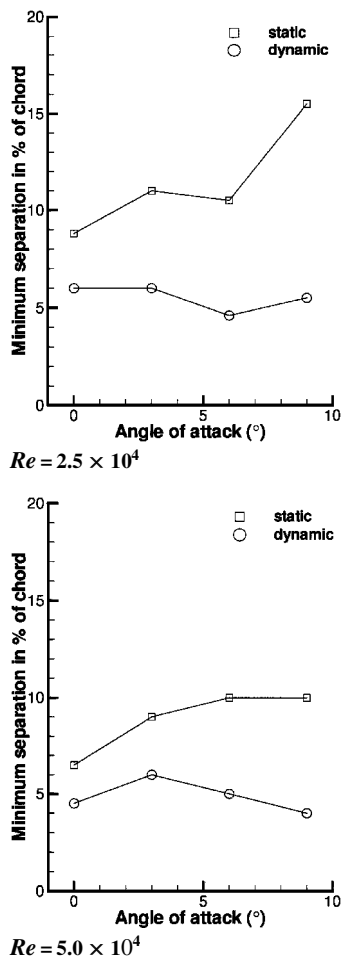


Fig. 4 Minimum separated flow thickness, static vs dynamic cases.

Measurements at a chord-based Reynolds number of  $2.5 \times 10^4$  show that the size of the separated flow is generally reduced with increasing frequency up to the point where normalization is lost. The measurements at  $\alpha = 0$  deg show a broad minimum around  $f^+ = 5$ . The measurement at  $\alpha = 3$  deg might also indicate a minimum before normalization is lost. At higher angles of attack though, where the decrease in separation is more significant, the improvement in performance appears to continue up to the point of loss of normalization. Past this point, where the amplitude of the actuator oscillation diminishes, the performance of the foil degrades at all angles of attack. It cannot be determined from present data whether this increase in separation is caused by the decreased amplitude or the increased frequency, but the former is suspected.

Observations at a Reynolds number of  $5.0 \times 10^4$  show no such degradation in performance past loss of normalization. In the non-normalized range the separation is in the range of 4–6% for all frequencies. In the normalized range the same general trend is seen where separation is reduced with increasing frequency. There is a possible shallow minimum at  $\alpha = 3$  deg and  $f^+ = 3$ , and another at  $\alpha = 6$  deg and  $f^+ = 3$ .

From a more detailed analysis of images such as shown in Fig. 1, it can be shown that the point of separation remains nearly the same when comparing the uncontrolled and controlled cases. Because the region of camber oscillation is downstream of the original separation point, this indicates that the actuation is not affecting the upstream flow but rather is aiding the flow in navigating the adverse pressure gradient in the region of separation, most probably by direct energization of the boundary layer. The flow examined here is within the transition range ( $Re \leq 5 \times 10^4$ ).<sup>1</sup> Transition can be located in the flow-visualization images and is not observed to significantly change chordwise location when the flow control is engaged.

Figure 4 shows the minimum observed separation for each combination of  $\alpha$  and  $Re$  for both the static and dynamic cases. It can be seen from this plot that the application of an oscillatory input holds the size of the separated flow to 4–6% of chord. This is, of course, more significant for the cases of higher angle of attack and for lower Reynolds number, where the nonactuated flow has a larger separated region. It remains to be seen if increasing amplitude will further improve performance in this range.

## Conclusions

Oscillating the curvature of the upper surface of a NACA 4415 airfoil has been shown through flow visualization to have a pronounced effect in reducing the degree of separation over a foil at the Reynolds numbers of  $2.5 \times 10^4$  and  $5 \times 10^4$ . Under these conditions the unmodified flow can separate by 0.15c or more. Separation, measured at the 70% chord position, was held to 0.04–0.06c under angles of attack up to 9 deg by oscillating the upper surface with an amplitude of 0.002c and reduced frequencies,  $f^+$ , ranging from 0 to 11. This represents a reduction in the separated flow size by 30–60% as compared to flow over a similarly shaped static wing. This technique shows significant promise, and it is expected that further tests will verify an improved efficiency in terms of L/D.

## Acknowledgment

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